

-480 1533 ✓ 18 10 00 -49 14.5 1009 +27



✓

✓

10.08 536 922 -143

2.26% Jeffrey

OpEx
revenue
10.08

48°15'32" 08 09 55 -49 13 10.83 +0.41

✓ 0113.66 11.64-11.5 " 1.4

1 more

10.74 -41.6(85) -370 2195 820774

+288 156 542 2650

R 4025 10.74
v0 11.53

-480,1530 08 09 55 -48 46 8.47+24

68494 ✓
FO I ✓

(X) 8.46 -552 937 -55 2.294 11472224
8.47 -556 943 -68 2.285 12'
8.46 -554 940 -62 2.290

67643 ✓
-4701466 8 06 10 -45 59.5 9.5

67643 ✓

67643 ✓

289 -354 854 -195 2.154 154 24

45

303 131 923 21.74
414 611

314 55

456 26

270 200

such one etc

40

(4)

up

-48° 15.34 08 10 00 -48 58 10.25-04

✓ /

E 0195

90 70° 90 150 45°
ABK

✓ 018 085 ✓ 306 ✓

2672

10.26 -670 806 -607

2.187 7m79

10.27 -673 803 -591

2.190 8 "

10.26 -672 804 -599

2.198

V 9.88

W -1.75 11.7°

CP = 100 x 0.2 49
10.2

67844

-150 3143 8 10 -46 04 9.2 42

48V

Q 9.45 -564 896 1157 2.308 24 2172
9.44 -556 901 +87 2244 20 0052
9.44 -560 845 +94 2.301

44 +136 171 1.021 2.807

(2) 213) (694)

1361 241 / 703 ✓ 1274

229

93

104 132 64 6029 2.815

369

1001

93

8.1

7.55
9.5
10.5

9 06 30 -47 625 8.7 -10

-47 18.4

-020 120 676 405 2.275

(1) (2)

8.64 -709 842 -240 2.277 18242

8.20 146 817 -217 2.275 24242

8.70 -702 830 -229 2.275

Round
✓

(3)

-013 105 688 2.275

(105) (69)

901

9.5

10.5

9.5

1901861

8 06 35 245 14 3.6 -0.2

9.71 -7.27 8.35 / -4.57 2.235 11.965
5.74 -7.14 8.20 -4.74 2.215 14.261
6.72 -7.20 8.27 -4.76 5 2.225
4.444 4.444 4.444 4.444 4.444 4.444
0.32 107 238 632 2720
0.044 0.044 0.044 0.044 0.044 0.044
9.55 9.55 9.55 9.55 9.55 9.55

67983

-4602176 8 07 45 -46 33 66 Fo

Fm S Jel

⑧ ~~Sat~~ 9.47 -51.3 945 -167 2.272 24 272 ✓

(11)

(12)

✓ 1855 214 752 2.284
⑩ 615
2.26 1855 214 752 2.284
6.1

✓ 1855 214 752 2.284
6.1

42

10.2

8 67 30 -47 18.5 ✓

-47° 1884

(+) 10.61 -642 887 +20 2345 2347
 (X) 10.56 -643 864 +52 2344 2347

(6)

(10)

044 449 676 2.676
 10.60 -642 877 +36 2366 2366 ②

050 153 961 2681

025 9 10.25
 10.55 -645 845 +55 10.15

10.15
 446
 → 9.55

8 05 50 47 54.5 10.5 42

4701916

(9) (40)

10.60 - 6.16 783 + 150 2.3609 415
10.60 6.17 901 + 118 2.375 1012.17
10.60 6.16 992 + 134 2.368

077 166 1062 2487

(10) 54

103
103
103
103

65248 H(1320)u

-41° 22' 12"

-41° 22' 12"

813

8.6
8.5 - 8

8.7 + 9.0

8.7 + 9.0
15.5
15.5
North component

✓ 08 45 -47 19.5 9.2 +50?

47.1615

1. ~~9.67~~ 9.67 9.67 9.67 9.67 9.67 9.67
~~350~~ 350 350 350 350 350 350
~~864~~ 864 864 864 864 864 864
~~429~~ 429 429 429 429 429 429
~~432~~ 432 432 432 432 432 432
~~432~~ 432 432 432 432 432 432
2. ~~328~~ 328 328 328 328 328 328
~~149~~ 149 149 149 149 149 149
~~478~~ 478 478 478 478 478 478
~~291~~ 291 291 291 291 291 291
~~413~~ 413 413 413 413 413 413
3. ~~9.67~~ 9.67 9.67 9.67 9.67 9.67 9.67
~~350~~ 350 350 350 350 350 350
~~864~~ 864 864 864 864 864 864
~~429~~ 429 429 429 429 429 429
~~365~~ 365 365 365 365 365 365
~~365~~ 365 365 365 365 365 365
4. ~~9.67~~ 9.67 9.67 9.67 9.67 9.67 9.67
~~350~~ 350 350 350 350 350 350
~~864~~ 864 864 864 864 864 864
~~429~~ 429 429 429 429 429 429
~~365~~ 365 365 365 365 365 365
~~365~~ 365 365 365 365 365 365

8 59 53 → 47 09 10,7 A2

-46 12225

(1)

$$\begin{array}{r} 10.51 - 6.19 \quad 979 + 236 \quad 0.36094777 \\ 10.46 - 6.01 \quad 859 + 234 \quad 2.375101977 \\ \hline 10.48 \quad 210 \quad 868 + 235 \quad 2.818 \end{array}$$

0.84 144 1.166 2.987

(181)

V0 10.15

10.2 / 9.85

69355 ✓
-4701626 7, 09 25 -47 45.5 8.0

8.13 -716 803 5 92 2.152 15260✓
8.10 -722 822 -607 2.184 13420 24
8.12 -710 812 -554 2.190 14100
~~8.12 -714 809 -556~~ 2.179
~~(83) 310 (476)~~ +154
8.11 -030 042 304 2671 ② (811 2.177
mV -176
g. 7 3

643645 (054) 8 09 25' 20 43.5 9.0 8.1
-4701924 7.9 1.76 679 0284 310 2.677

4701924 - 716 803 - 592 2.162 172102

(+) 110

4502257 8 11 50 44 13 8.5³+ml?

4502257 8 11 50 44 13 8.5³+ml?
4502257 8 11 50 44 13 8.5³+ml?

4502257 8 11 50 44 13 8.5³+ml?

4502257 8 11 50 44 13 8.5³+ml?

050 450 950 2.522

4502257 8 11 50 44 13 8.5³+ml?

4502257 8 11 50 44 13 8.5³+ml?

18825

45°22'49" 8 11 30 ~45 47.5 8.1 BF

B3^{IV}
BF

(A) ①

8.75-704 772-143 2.164 20m/s ✓

8.76-705 772-124 2.15921m/s ✓

8.76 704 777 135 2.162 ②

65724
4612245

822/8 III/d
8 11 00 47 17.5 9.5 B.S.

9.60 499 257 - 554 2.196 20 Nov 97
~~9.61 652 798 - 617 2.174 27 Nov 97~~
~~9.61 - 704 799 - 614 2.185 30 Nov 97~~
~~9.61 + 643 794 - 617 2.154~~
9.61 646 - 604 0.25 297 2.667
9.25 674 2.94
9.25 674 2.94
9.25 674 2.94

Em:
B35V_{Ma}

14.5

-46.02306

8

64404

⑦ 6.48-C50 84 (-700 2.139 254.5)

W

⑧ 6.22

10. 0.25 1.52

(146) 315 6.5

64354

-4602361

8 14 07 246 09 9.0 B/S
-4602361

84/5 DV

1469 927-204 885-640 2.164 21masr

N₃ ②

64355

-412289 81100 -45 59 9.283

(+) 9.56 - 6.50 220 - 532 2.170 21 MAY

2513/18

69534
-1702018

Open
8

28.5 48/F2
-47 96 A2

9.43 -562 891 +176 2.346 301472
9.50 -563 920 +156 2.366
10.03 -565 905 +160 2.330 22Mn72
9.6 -567 908 +177 2.340

① 100 173 1.104 2.840

150 9.19 -673 806 -234 2.214 21Mn72

14 24
110 4048 9.75
11.75 85 236875 +2.5

-4413714

8 31 15

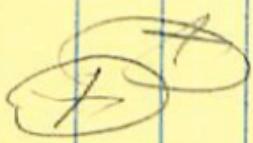
-45 04.55 16.788



64541

A2B

-460 2319 8 14 50 -46 59 86 AD



9.16 -618 909 +105 2.365

9.14 -604 915 +151 2.352 - 21 mm ✓

9.15 -611 913 +180 2.354

9.0 082 185 1058 2.875

(2.8) 104 ✓

(641)

9.5 141 1036 2993 905 (426) ✓
70 222 137 423 9.05 ✓
70 222 137 423 9.05 ✓

67611 ✓

-4101464 8 06 00 -~~18~~ 43 9.5

F2 III/12

(A)

9.45 -414 874 -326 2137 1574 76

9.4 384 174 586 2483

226 580

347
3 347
347
347

33

A9 E

67584 ✓

-48 1461 8 05 50 -~~48~~ 44 10.1

77 money

10.27 -524 925 +23 2332 1509.74

16.6 156 94.6 2844 (175)

6.5
1.655 10.1
7.5 (246) 614

234 434 2.42
7.2 2.6 7.5