

0.31 1280

26.7-1 23.54 -35 -29 13 9.5 +3

8.32 +0.945 +0.73 17 2470

981441

1779821

0.24 2730

266-19 23 57 42 -26 13 11.2 + 3

8.75 +1.08 +0.85 17 Sept 23



terne

Prese  
Prese  
Prese  
Prese

Prese  
Prese  
Prese  
Prese

7.52 10.72 + 0.32  
10.72 10.32

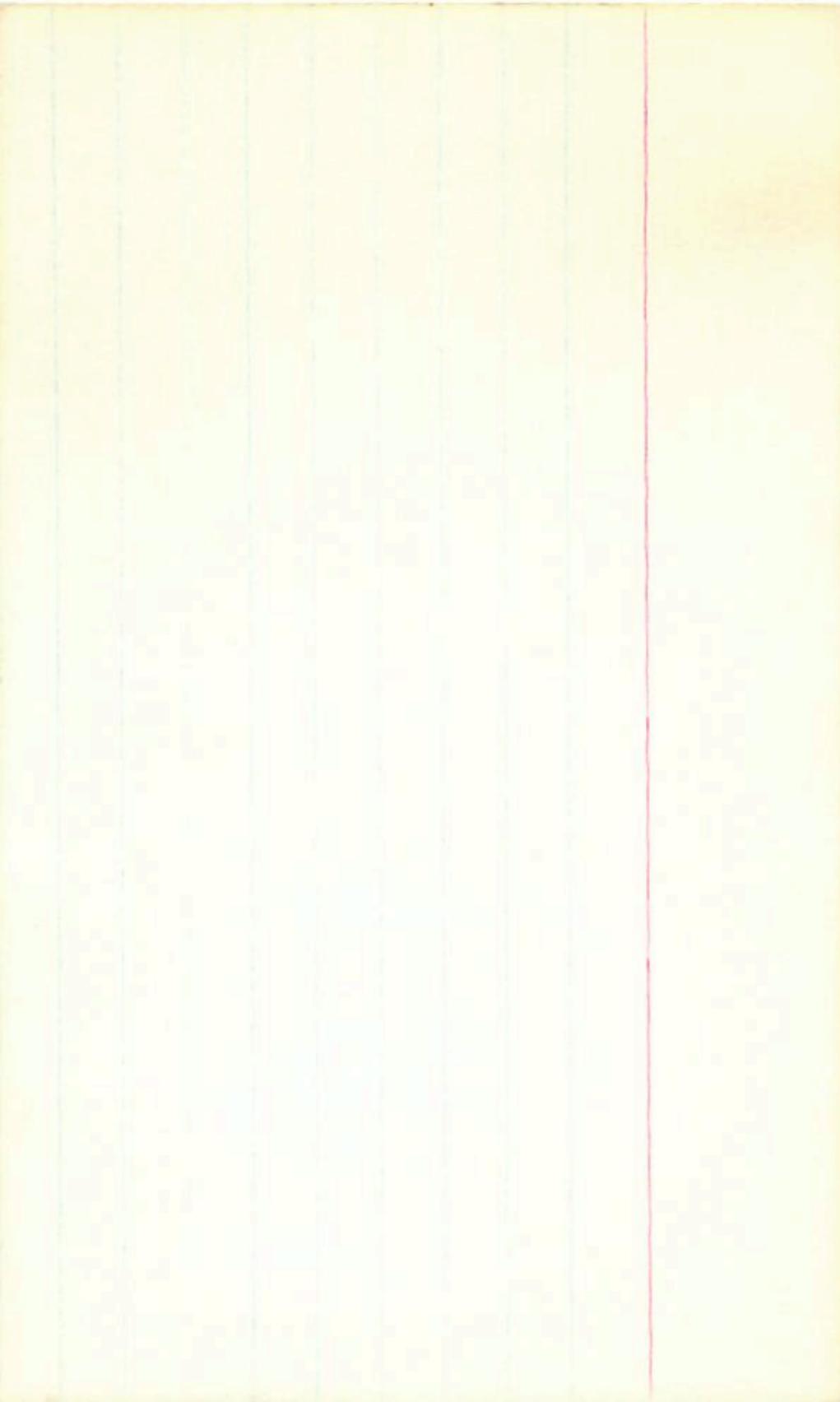
266-21

266-21

266-21

0.56 1210

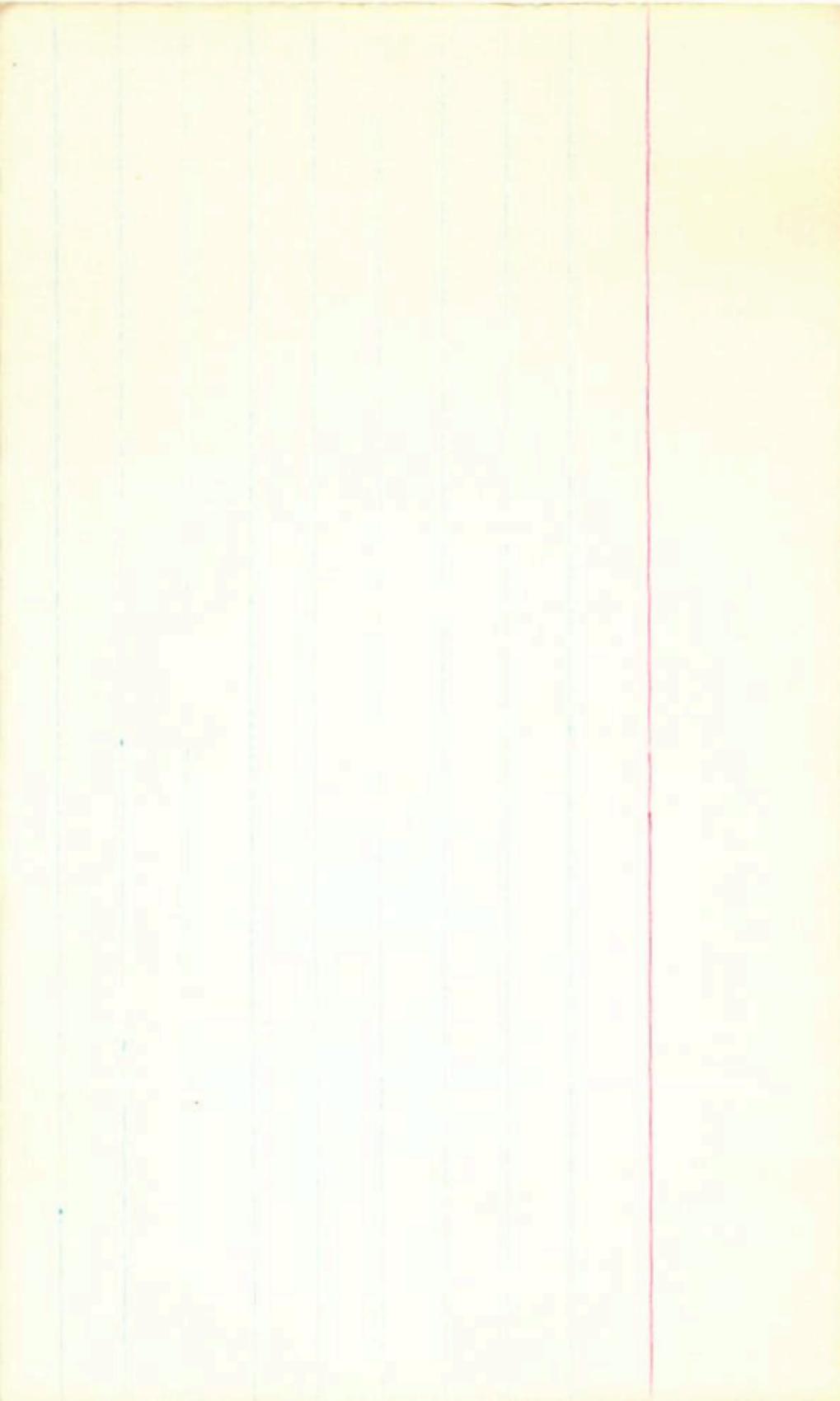
0.56 1210



L77 98444 0.40 1000

267-12 23 57 120 -85 20 13.443

12.32 +147 +1.225 17 Sept 22



CRI 23 55 20 -23 36.5' 12.0 + Y

9.43 +1.045 +0.97 81 Aug 73 9.07 +0.412 854 +73



May

0.11 195° 40

132 0

60 578

62 20

24 -30 56

12.94 10.15 +6.68 17.54 +13

0.20 920

266-28 02 00 15 -20 015 126-13

1/24 10.875 times ♀ Sept 23

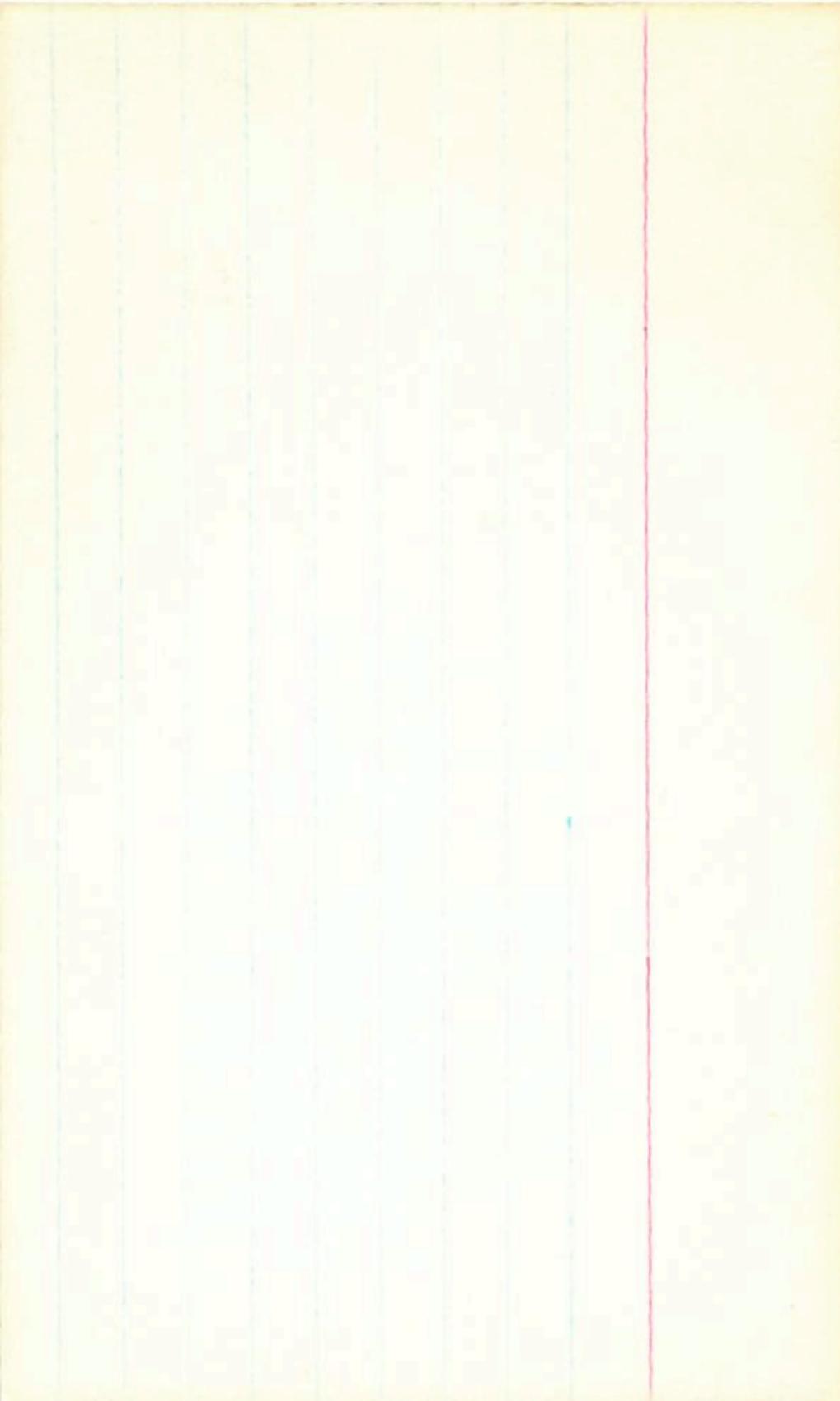


LTT 12

0.30 1156  
.30 125

6266-33 62 02 09 -28 34 28 03  
6267-21 10.2 +2

8.30 +0.775 +0.365 17 Sep 23  
6.25 +0.76 +0.42 1 Wind



0.22 216.0  
1.24 246

626.6-85 (v) 02 44 -24 05 11.8 +3  
267-2n

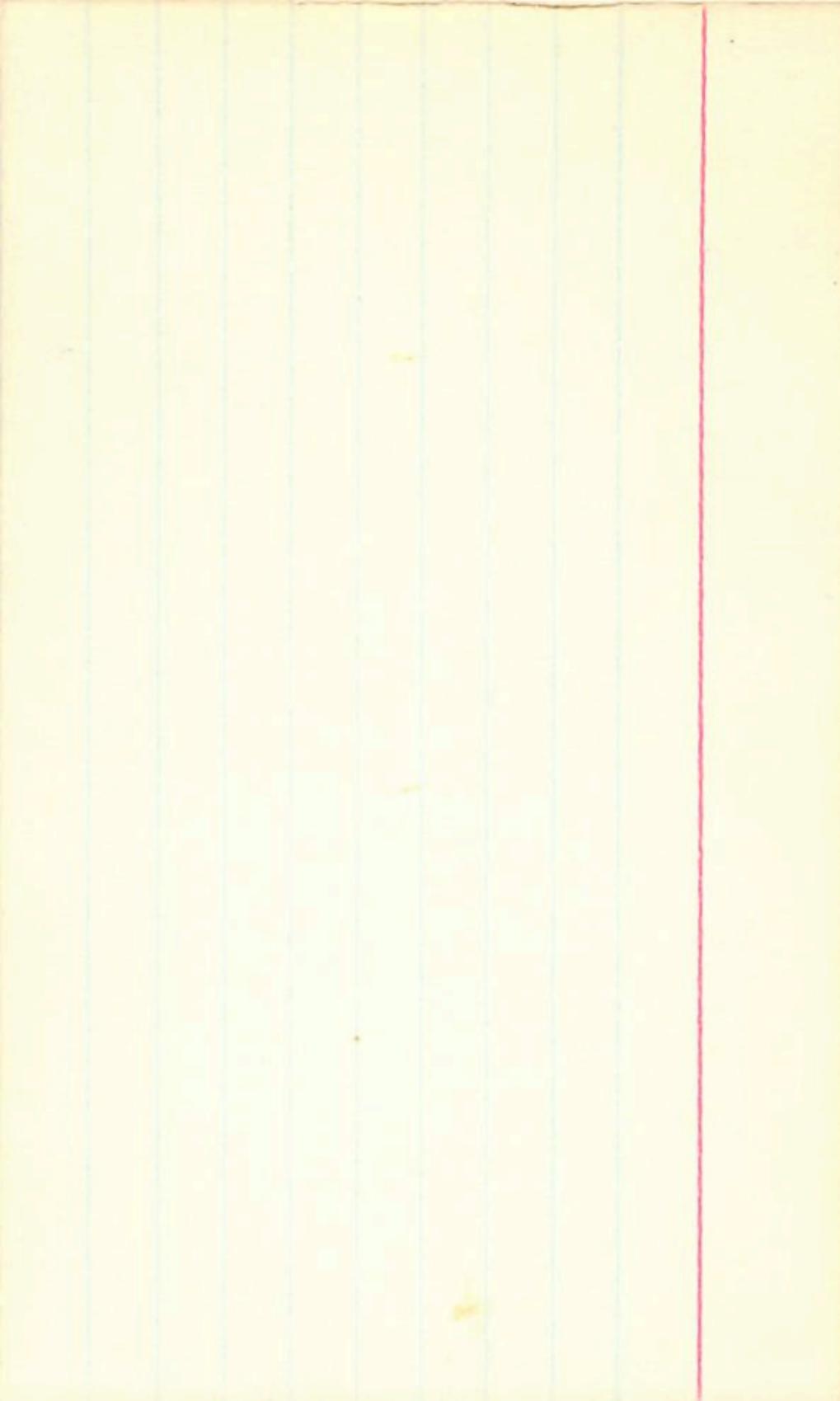
96.5 ✓ +0.74 +0.19 17 Sept 73  
8.110 +0.75 +0.21 3 Wind



266 - 36 652 03 10 -28 30 143 159  
159 159 159

13.41 + 1.45 + 1.25 17 total

12.42 + 6.43 14 total



17729

0.21 850

264-37 65 03 55 -26 68.5 137+3

12.24 11.11 10.99 11.22



.20

26.43      07 05 32 - 25 34 17      16.5 + 03  
15.7 mm

14.95 + 1.62 - 17 Oct 73

13.50 + 1.11 (18 Oct 73)

657

July 34 03 10 23 30 15.9 + 3  
14.95 + 1.0 - 17.00  
w-10 k-m

210 w

880-4400 020 05 35 -29 43 12.7 h  
64.6 -29 50

11.02 +0.50 23 Nov

LTT 47 0.34 720

Jul - 48 60 06 00 - 23 54 9.5 + 3

8.75 + 6.80 to 30 n Sod 22



0.20 1260

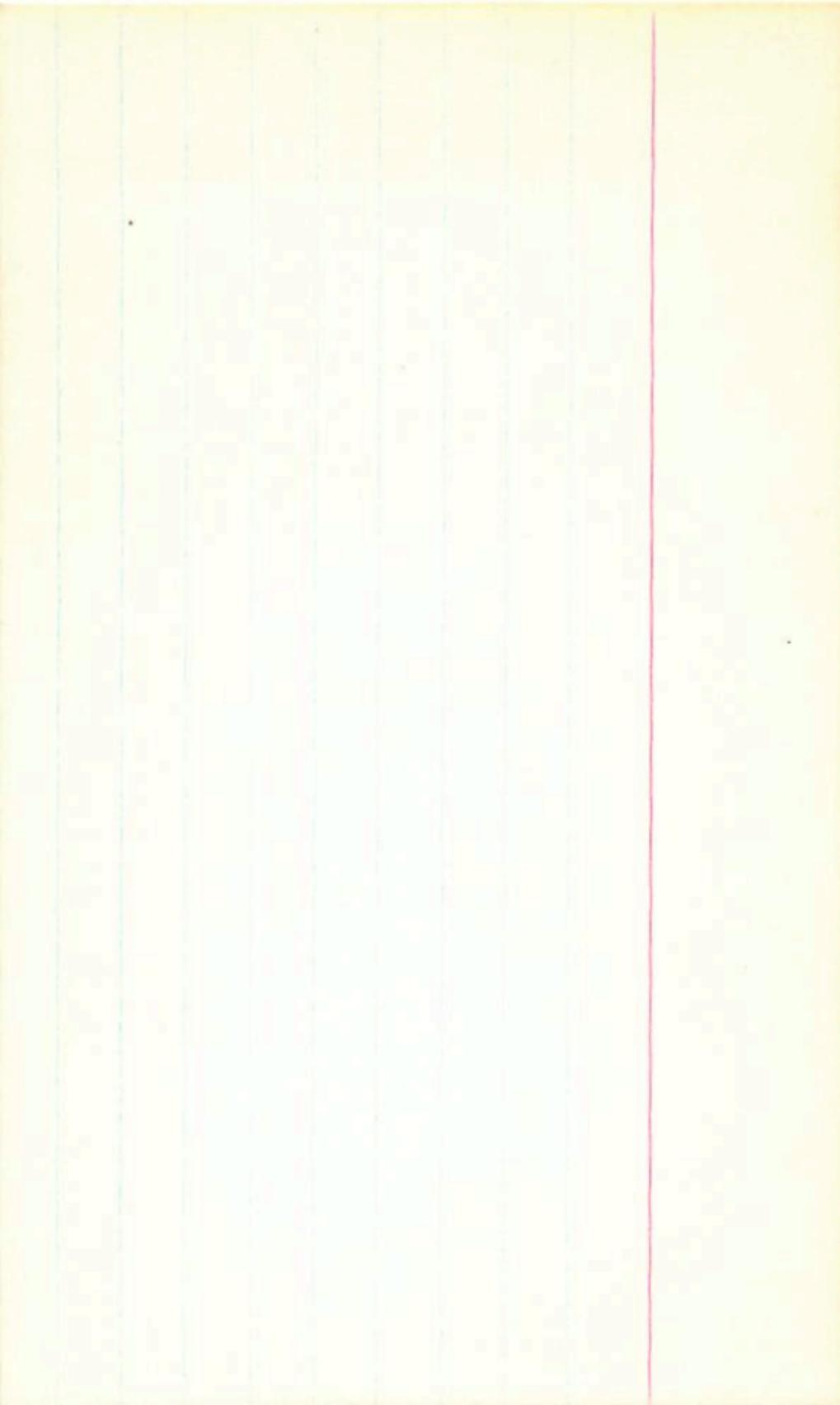
264-53 67 07 07 -20 34 / 3.1 t3

1145 +0.96 +0.24 m sup 2



880.531      0      04      06      27      57      14.6      h.20

13.13      40.5      15      20  
21



LFT 78 0.72 1030

26.745 070 10 09 -39 24 ~~62.4~~ +3

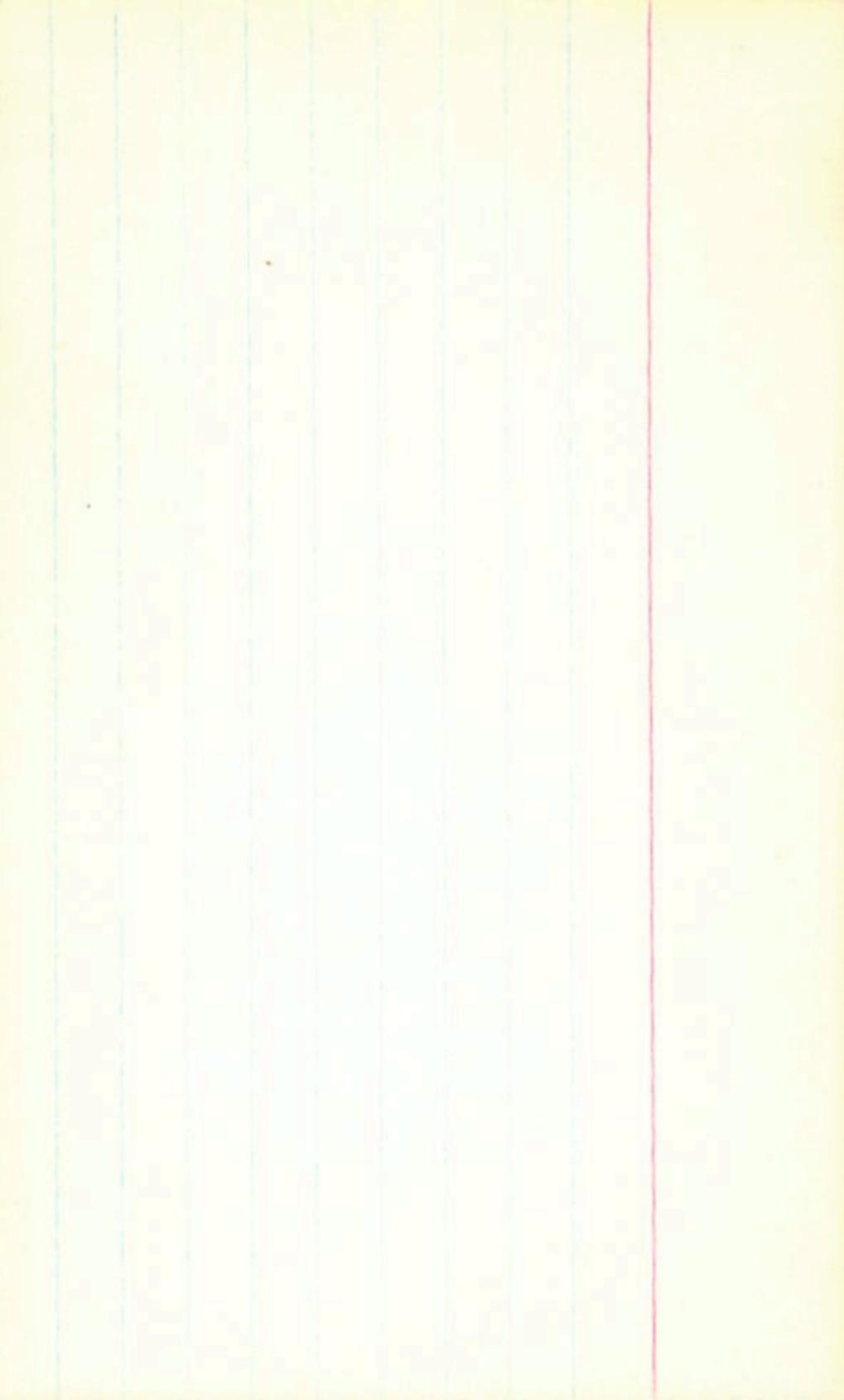
10.05 +1.05 +0.52 1754.73



LTT 95 0.42 216.0

267-53 02 11 58 -87 02 127+3

16.85 +144 +1.185 17 Sept 23



Can 3 070 14 03 -15 31.5 16.1 +4

13.57 +0.72 18 Sept 3

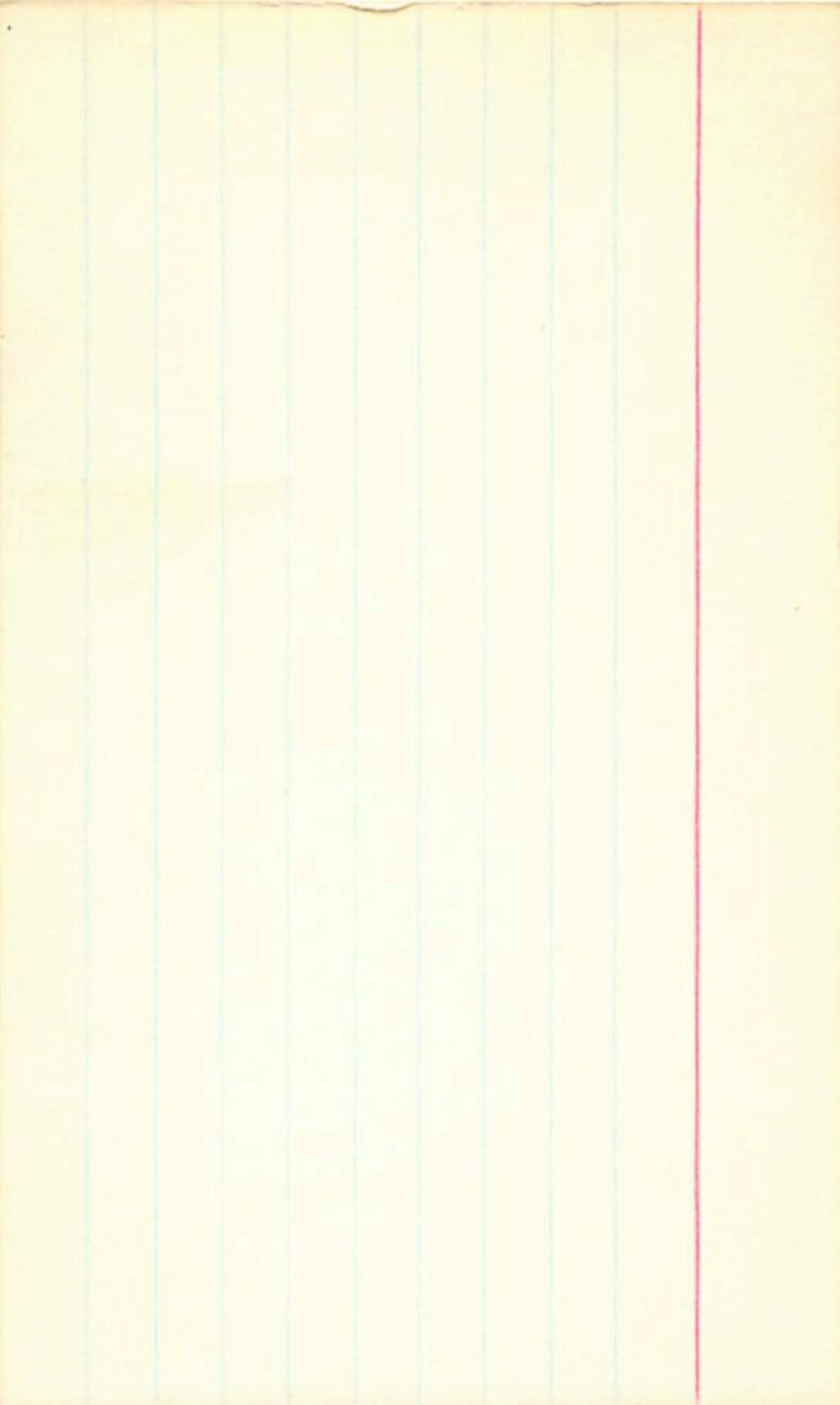
764-92

264-83 02) 16 22 -18 04.5 149+3

13.20 1158 - 1160.973

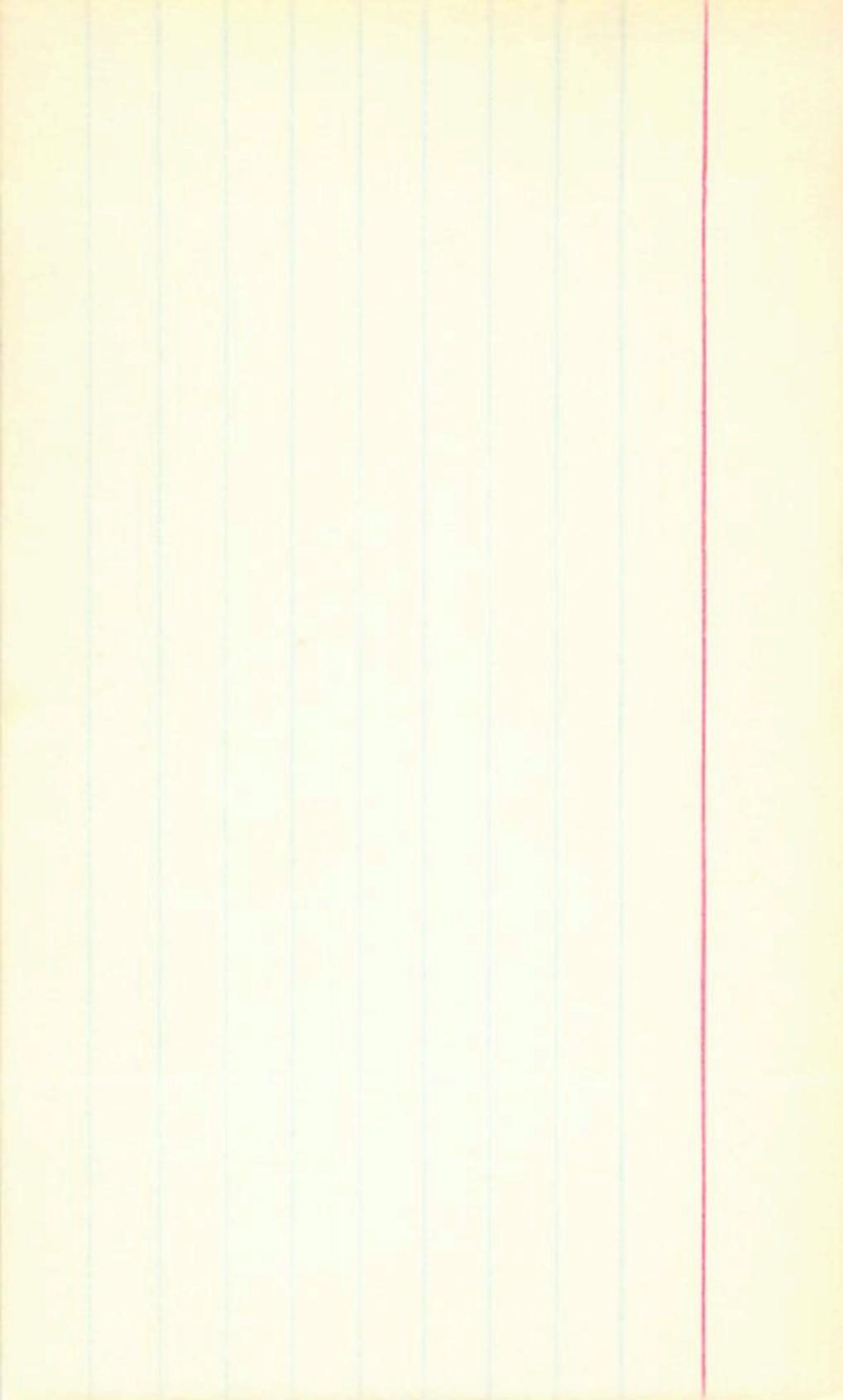
.27 - 225 3.4 km

11.48 + 1.095 136ut  
23



266-87 00 17 44 -20 05 14.7 +3  
12.50 +1.55 - 11 last 73

11.52 +0.775 14 last 23



764-1118

GPF

00 18 36

17 14

12.4 m 116D

10.87 18.835 33S<sup>ft</sup> 7.3

618 00 23 47 - 16 34 15.5 + 4

12. ~~80~~<sup>80</sup> ~~166~~ (83.67)



to.

13.38 + 10.5 ✓ 18 Sept 3

12.80 + 0.905 ✓ 18 Sept 23

121

15.5 + 3 .33 "

266 - 122 ✓ 11 28 29 117 ✓ 16.1 + 4

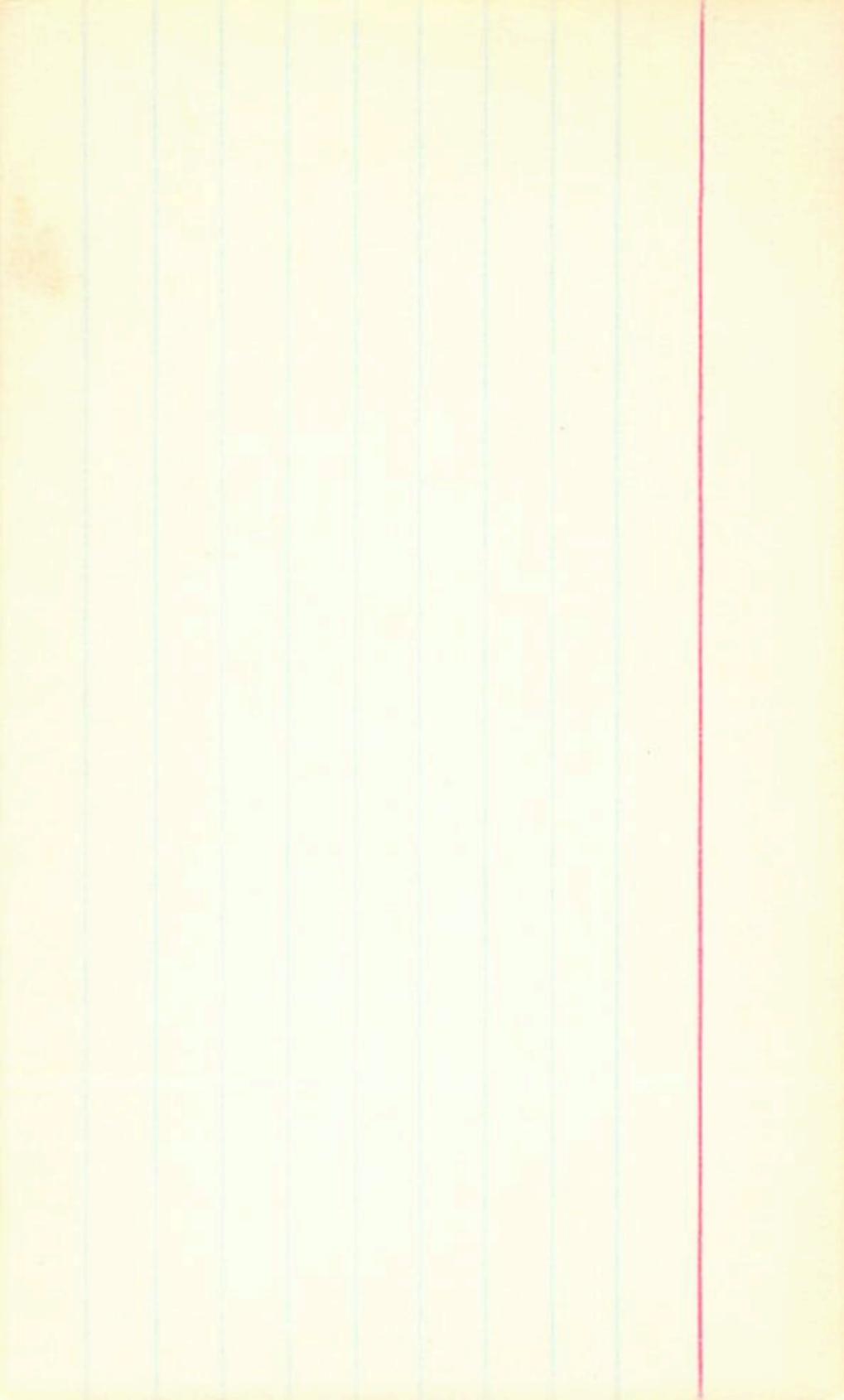
✓ 129 970



, 51

247-126 60 31 23 -34 56 / 43 + 3  
                

12.35 + 0.385  $\overline{1464}$   
23



. 17)

268.5      00) 39 34 - 16 47.5      16343  
152 m .46

1343 + 1.005 22675

268-83

071 55 22 -17 31 15.243

13.38 10.53 2100.5



264-65

264-65 57 14 -37 30 132+2.122

1654 + 0.455 = 0.165 8 nov 22

2764-69 12.4 42 0.200 670

Gp 23 01 00 51 47 11 15.7 +4

13,69 + 0.4 / 18 S<sub>4,5</sub>?



264-81 01 61 30 -37 28 10.1 t<sub>2</sub> ,24

$$8.51 + 0.58 \sqrt{-0.025} \quad 8 \text{ m/s}$$
$$8.51 + 0.58 + 0.02 \quad 3 \text{ with}$$

0.21 2090

268704    0102    20    77    10    15.9+4

12.56 +613 1852  
23

LTT 625

" 25 1560

269-98 01 05 00 -86 55 12.2 +3

10.18 +1.00 +0.91 175<sup>2</sup> 73 9.63 +0.86 185<sup>2</sup>  
10.11 +1.05 +0.93 2nd



LTT 633 0.40 107.0

26.8 - 11.9 01 05 50 -17 47 12.7 +3

11.29 + 1.20 + 1.16 + 1.50 Sept 23

10.50 10.535 18 Sept

Now

6.35 2050 LTT 436

6.268-122 1.06 0.3 -15 40 13.6 +4

12.36 +142 +1.21 17 Sub 72

11.57 +0.70 384  
11.37 +0.685 1854  
11.47 +0.69



0.52 360

218-128 01 07 27 -15 07 15-44

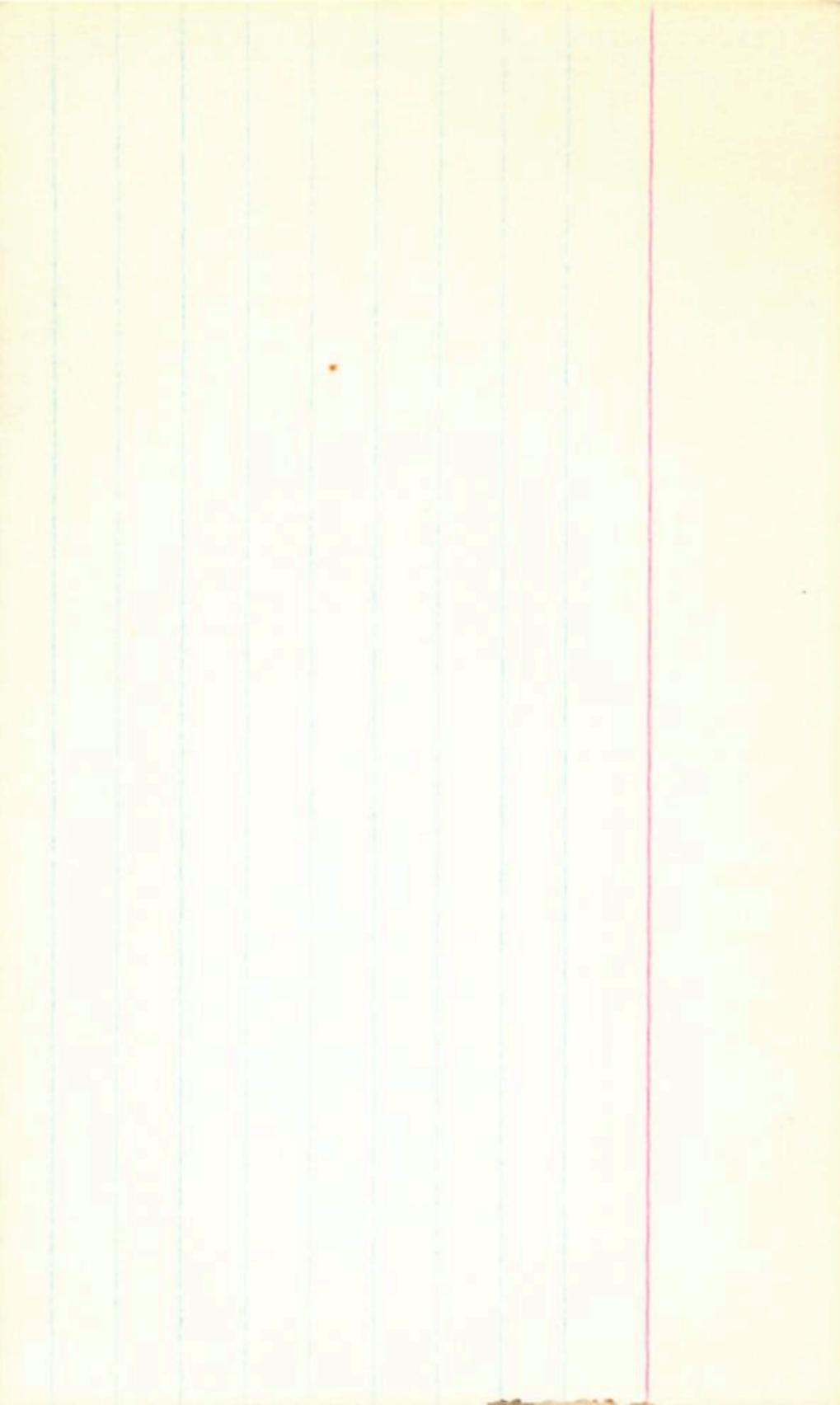
1253 4105 / 1854  
23



61729

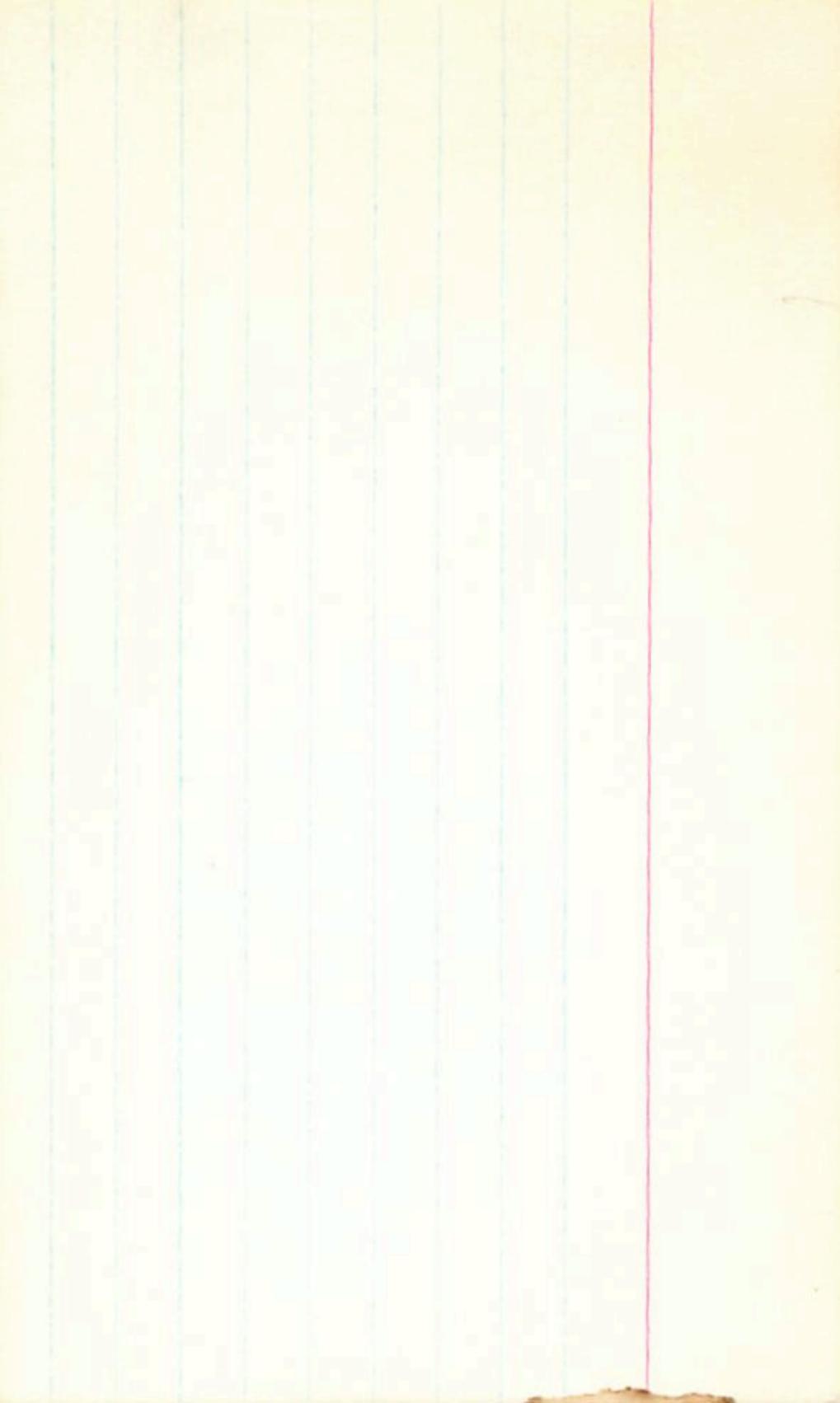
01 08 27 -15 20 16.7 +4

13.63 +1.27 854.62



GR 30 0109 01 -15 20 16.1 +4

12.94 11.25 3 Sy 13



Can 31      1 09 14 -18 09 16.1 +4

767-774      14.4 m .194

1336 1681 3544  
22

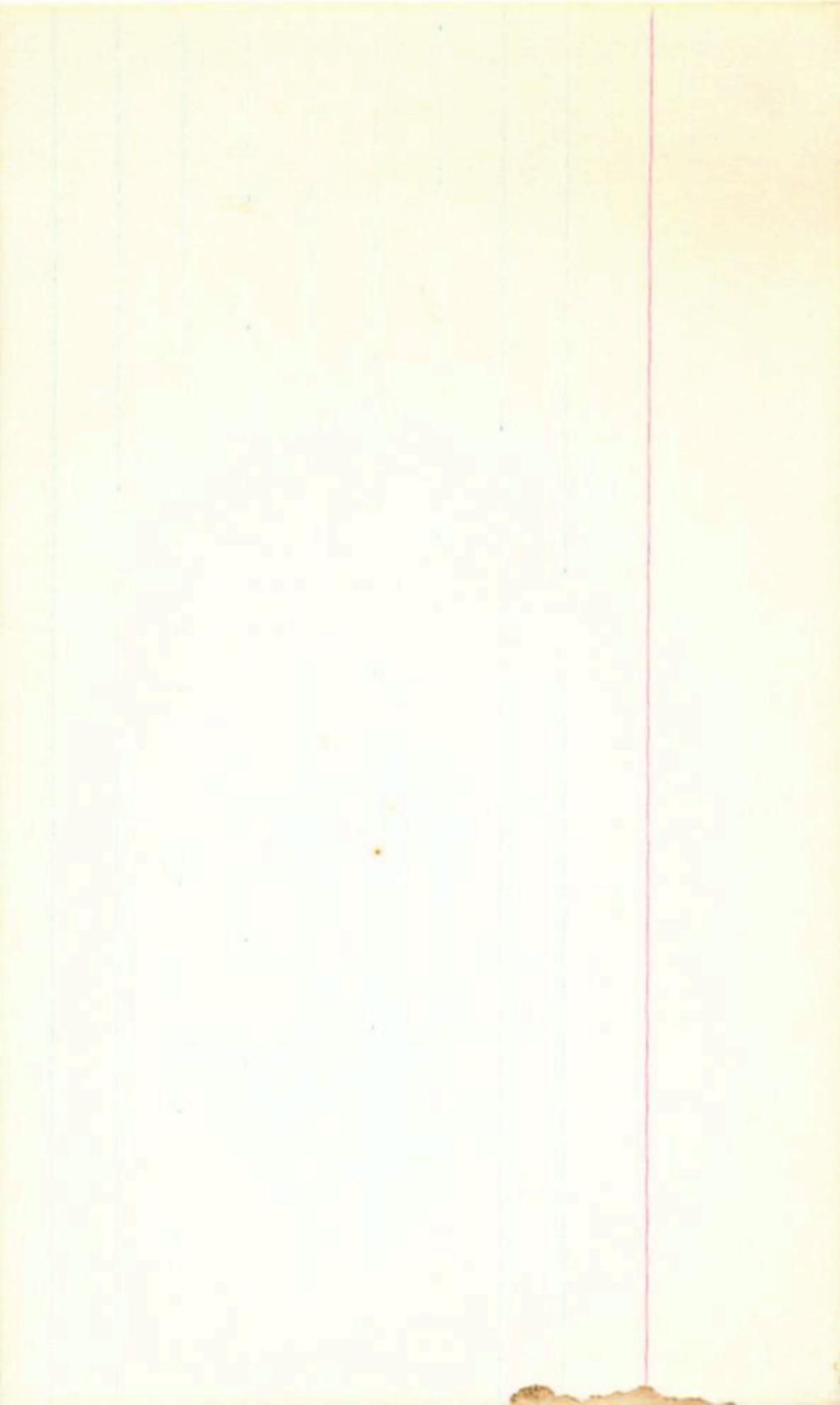


~~619.32~~

~~628.2~~

1 69 45 -14 15 169 + 4

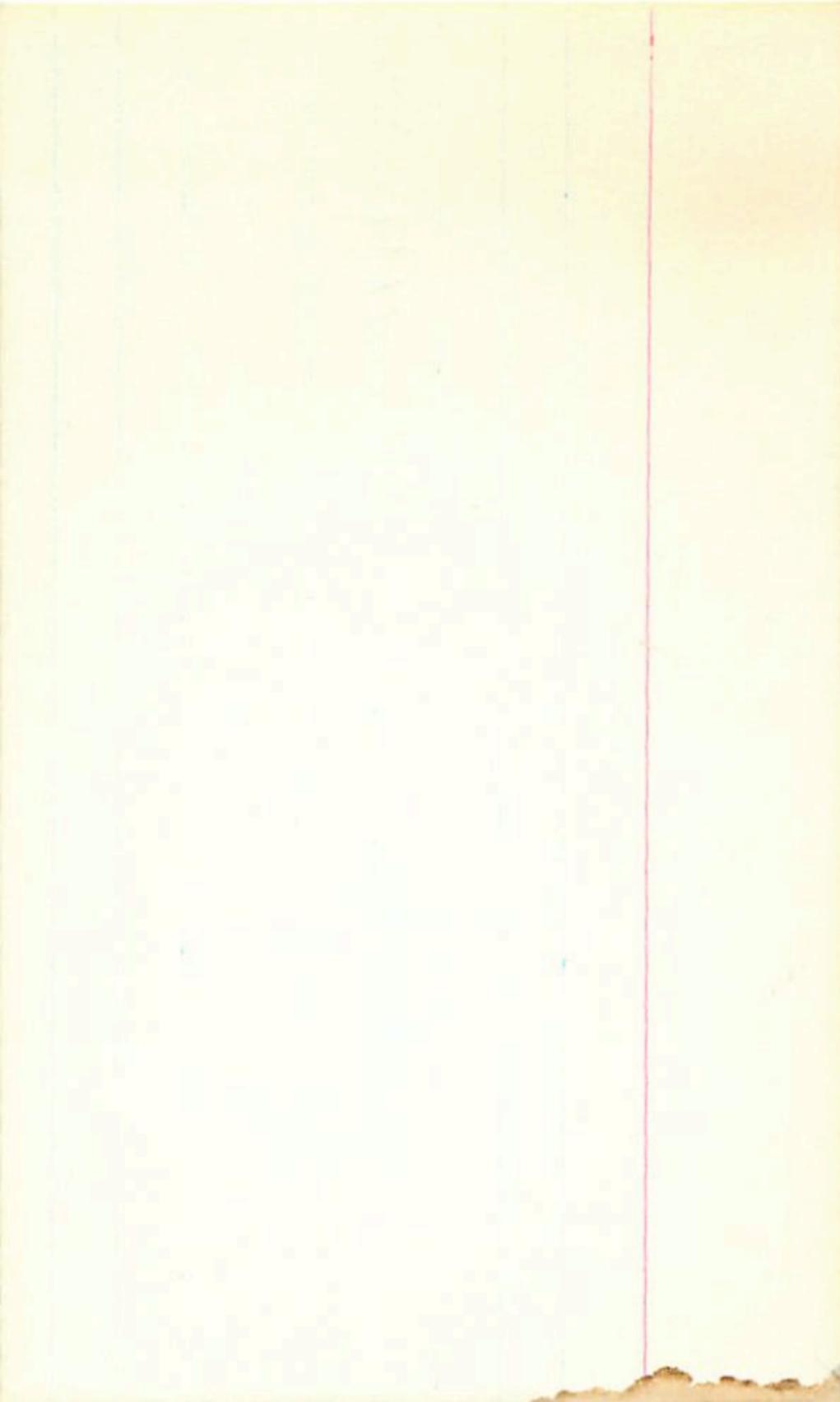
13. 55 10.78 354.2



~~6264-125~~ 1 12 49 37 56 144 44

1345 +1665 +1.835 81 May 73

~~12.49~~ +1.175 854.73  
12.49



0.251 2120

265 mm 01 14 05 211 m 15.2 + 1

12.29 +0.68 1850ft

12.29

~~21st~~ — 067-215-07

" 0.221620

26.4-18.3 61 15 50 -35 52 18.2-23

11.42+1.53 +1.19 17 Sept 22

10.80 40.56 \$ 18.84

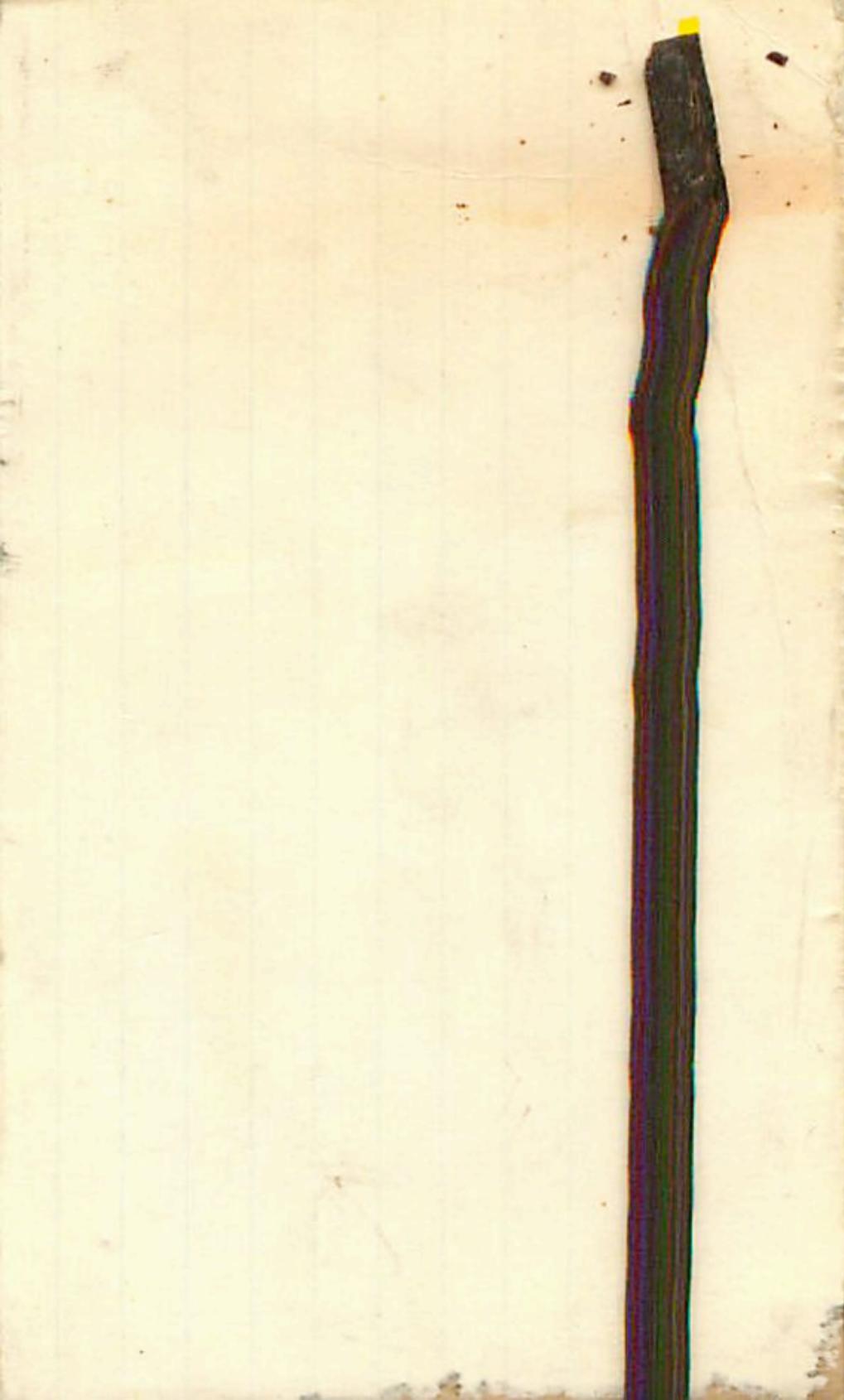


6172

120

269-172 01 27 52 - 33 47.5 13.5+2

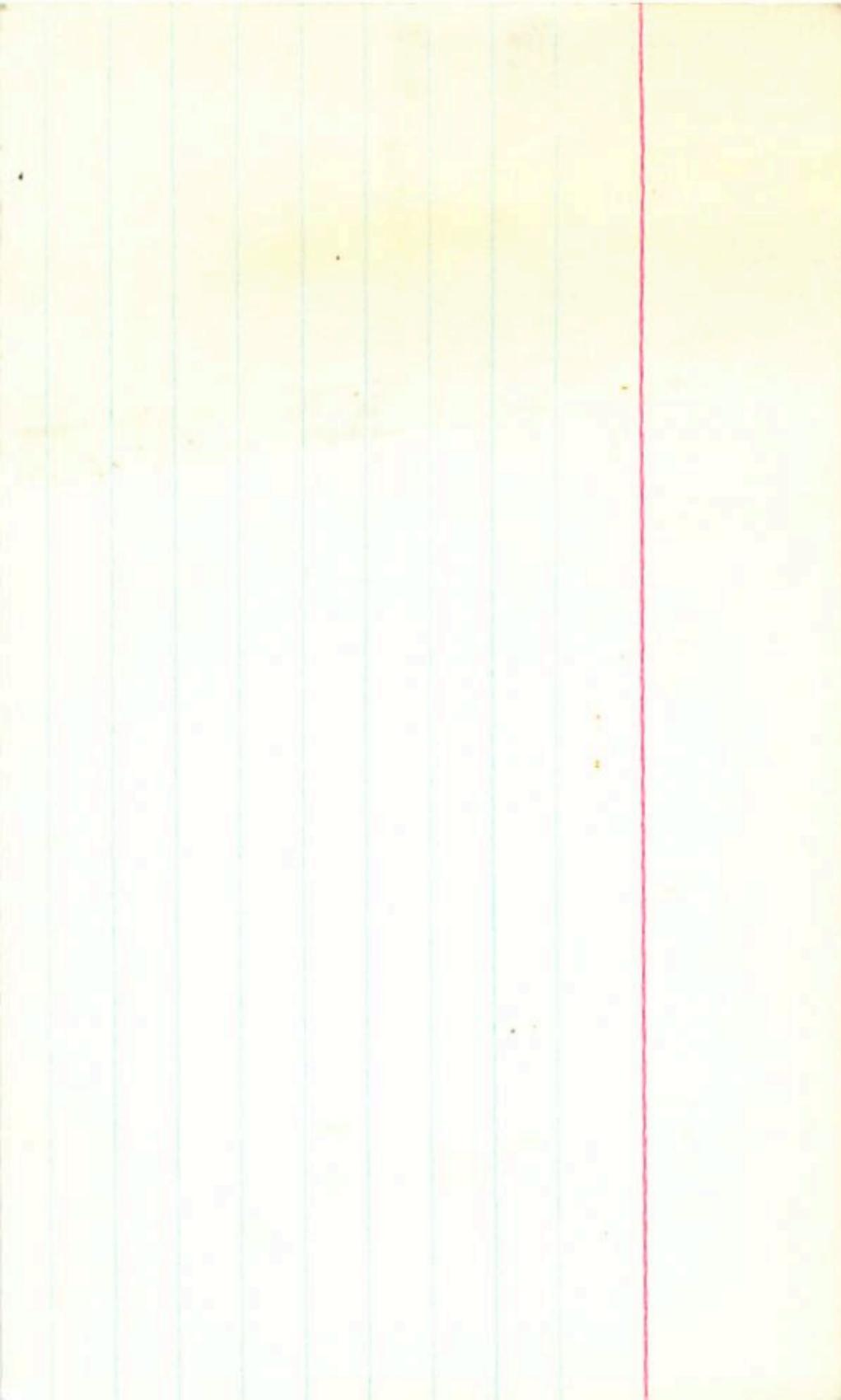
10.54 10.565 13 mm 25



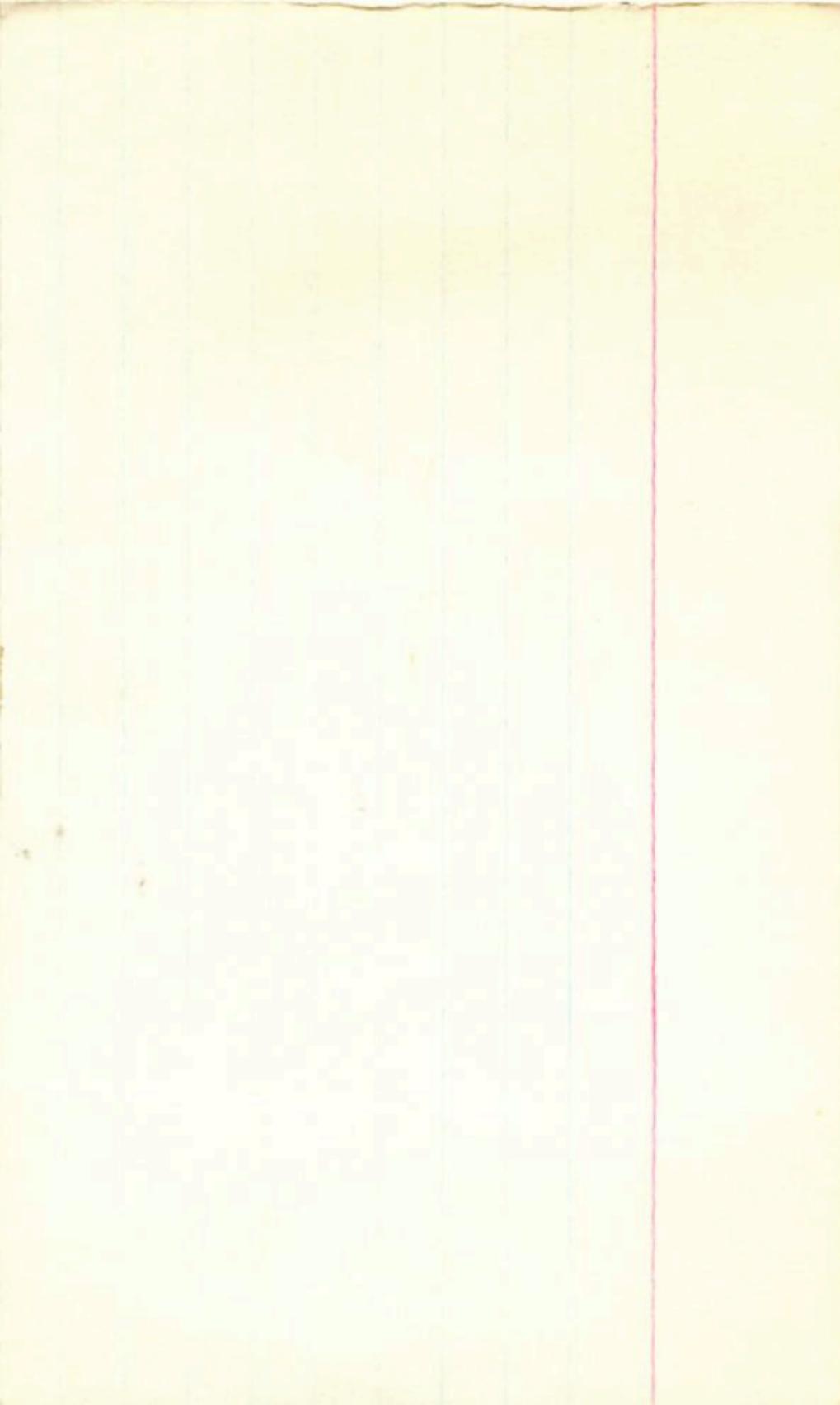
100%

880-546 00 08 40 -27 30

145 15.8 km 0.224 67



075 09 57 -28 21 12.0050/65  
11.51 +0.74 10.245  
89874

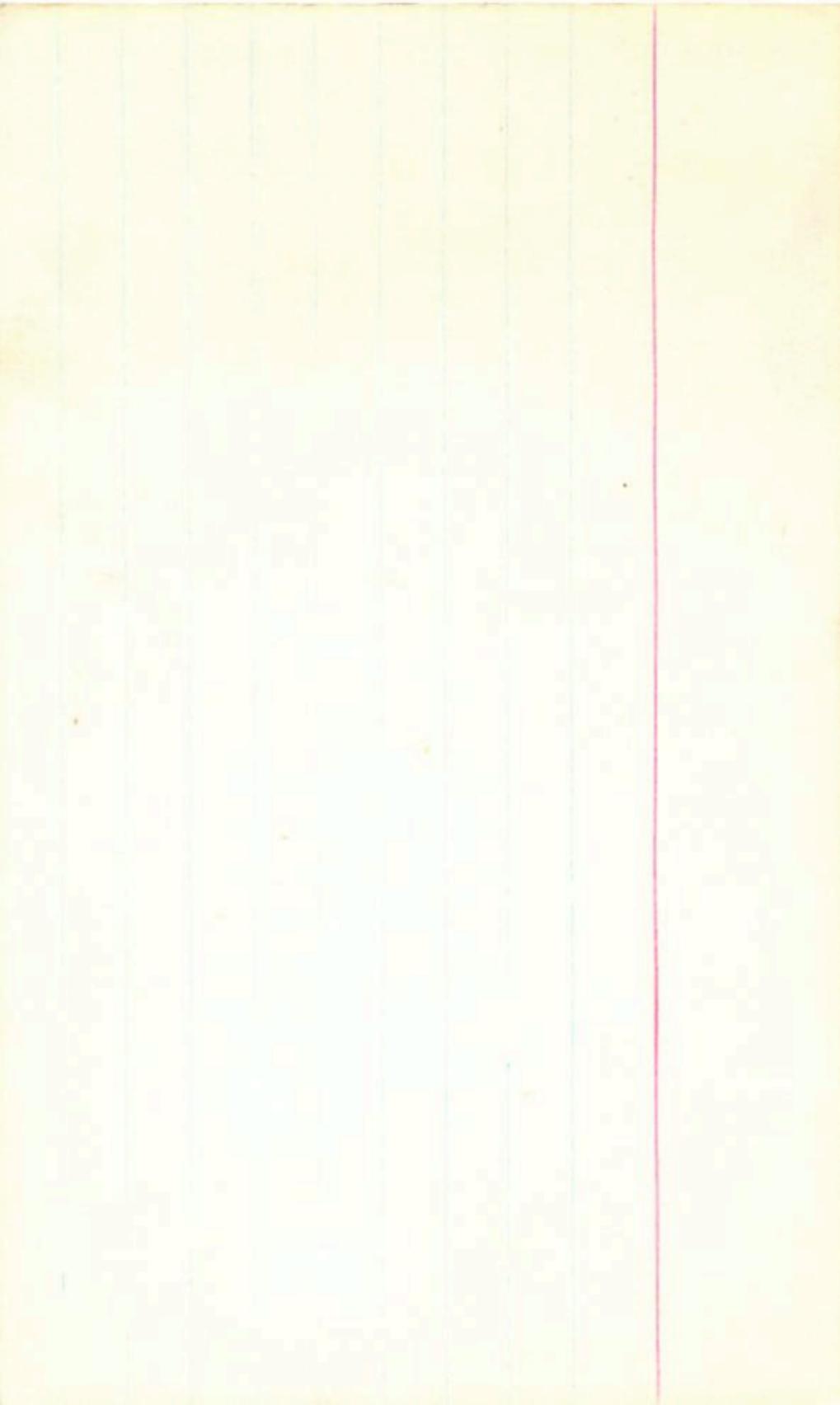


B

No Blue

175 00 15 51 -25 08 122.05%  
175 00 15 51 -25 08 122.05%  
175 00 15 51 -25 08 122.05%

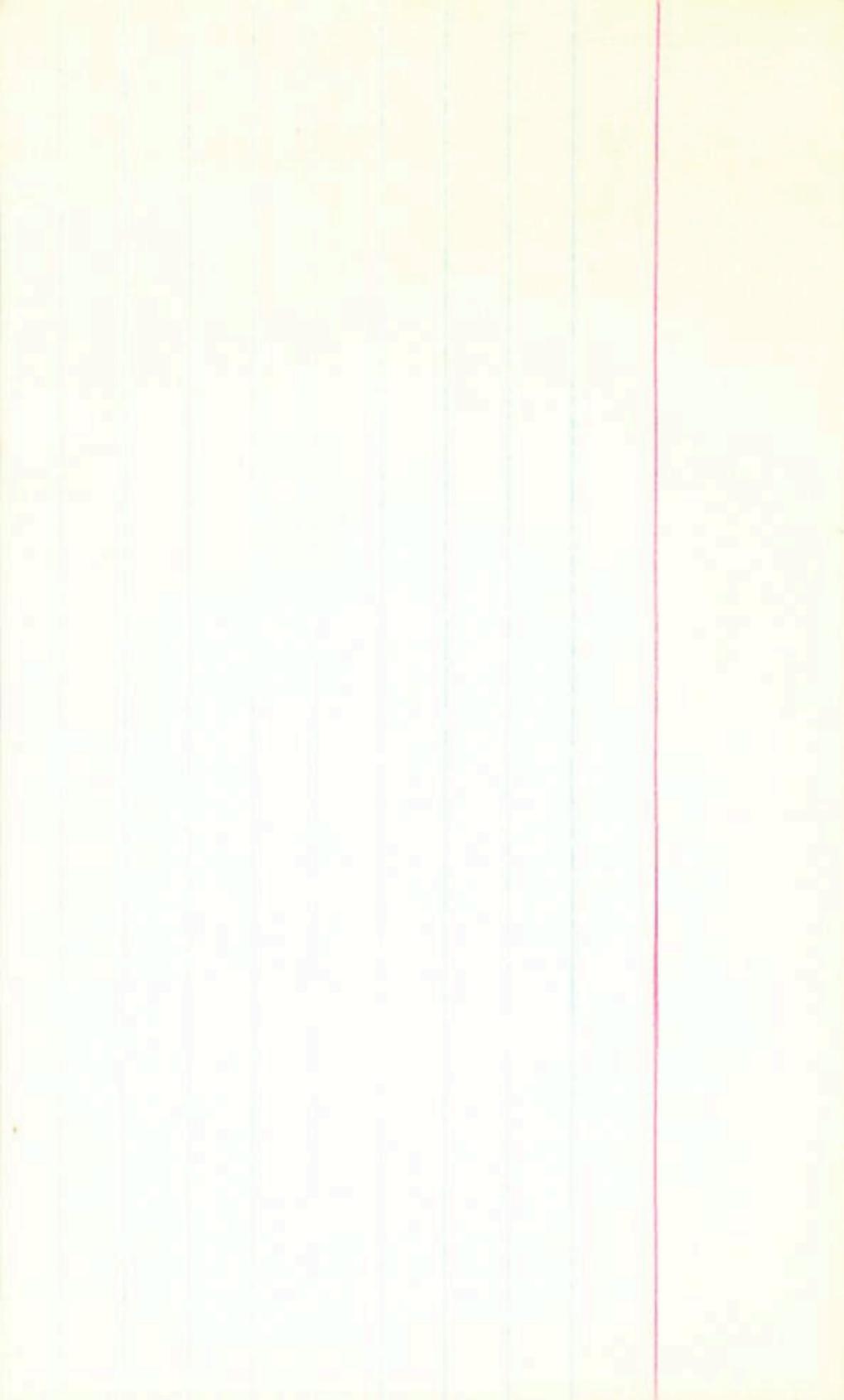
1162 +0.665 ✓ 10.17 13/2974



165

52 17 03 30 02 11.7 0955 2240

11.56 +0.805 -0.405  
298.74



1

255      50    21    24    -22    41    13.3 050 1150

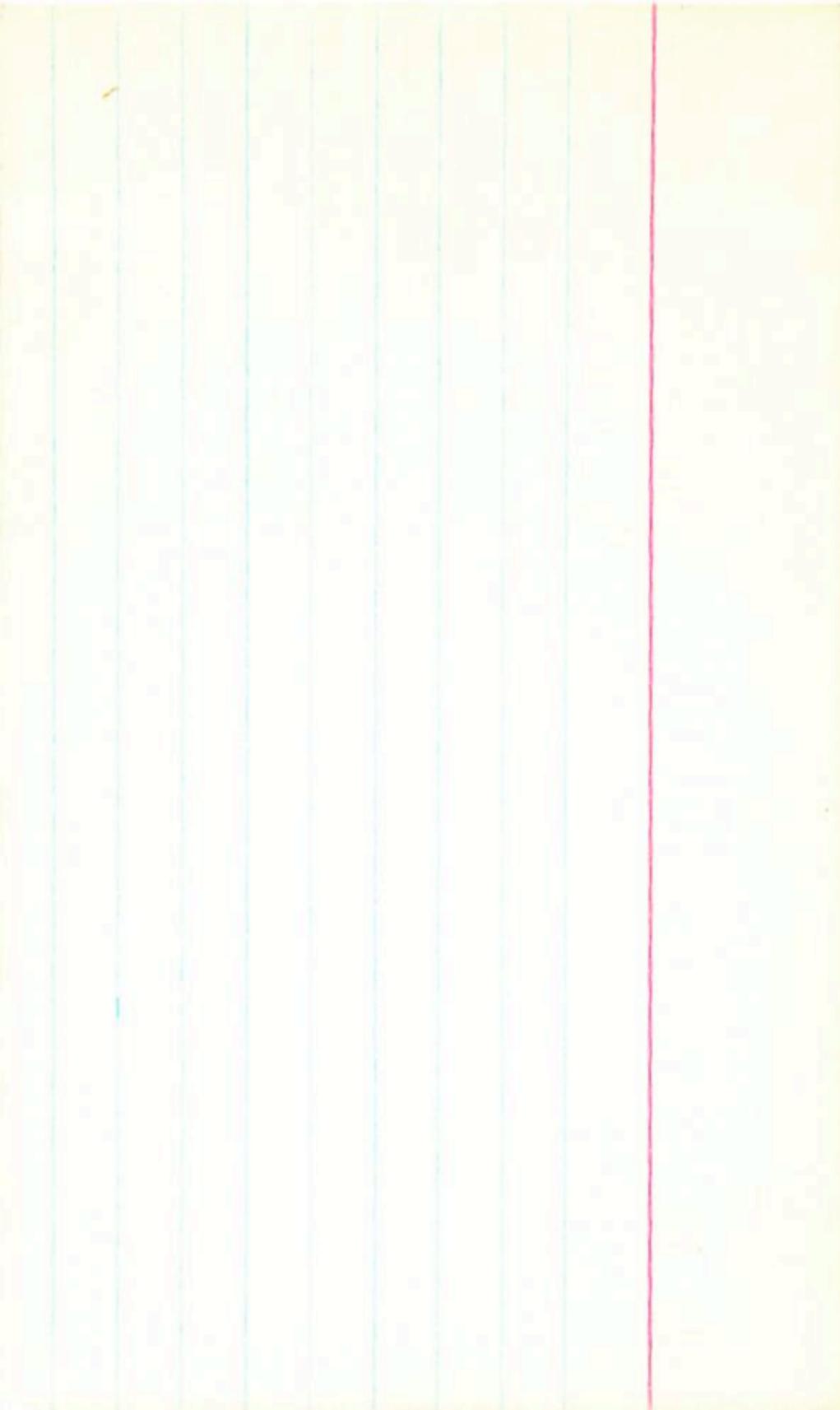
12.61 + 0.825 + 0.425 13.874

① ✓

~~46,274/25 60 22 39 - 21 24 (13.9 053 250~~  
80" MP (14.5 053 250  
✓ ✓  
~~12.09 10.89 10.515~~

13.98 11.16 10.845 1.02  
77

7 13.20 10.24 5.0274



846392

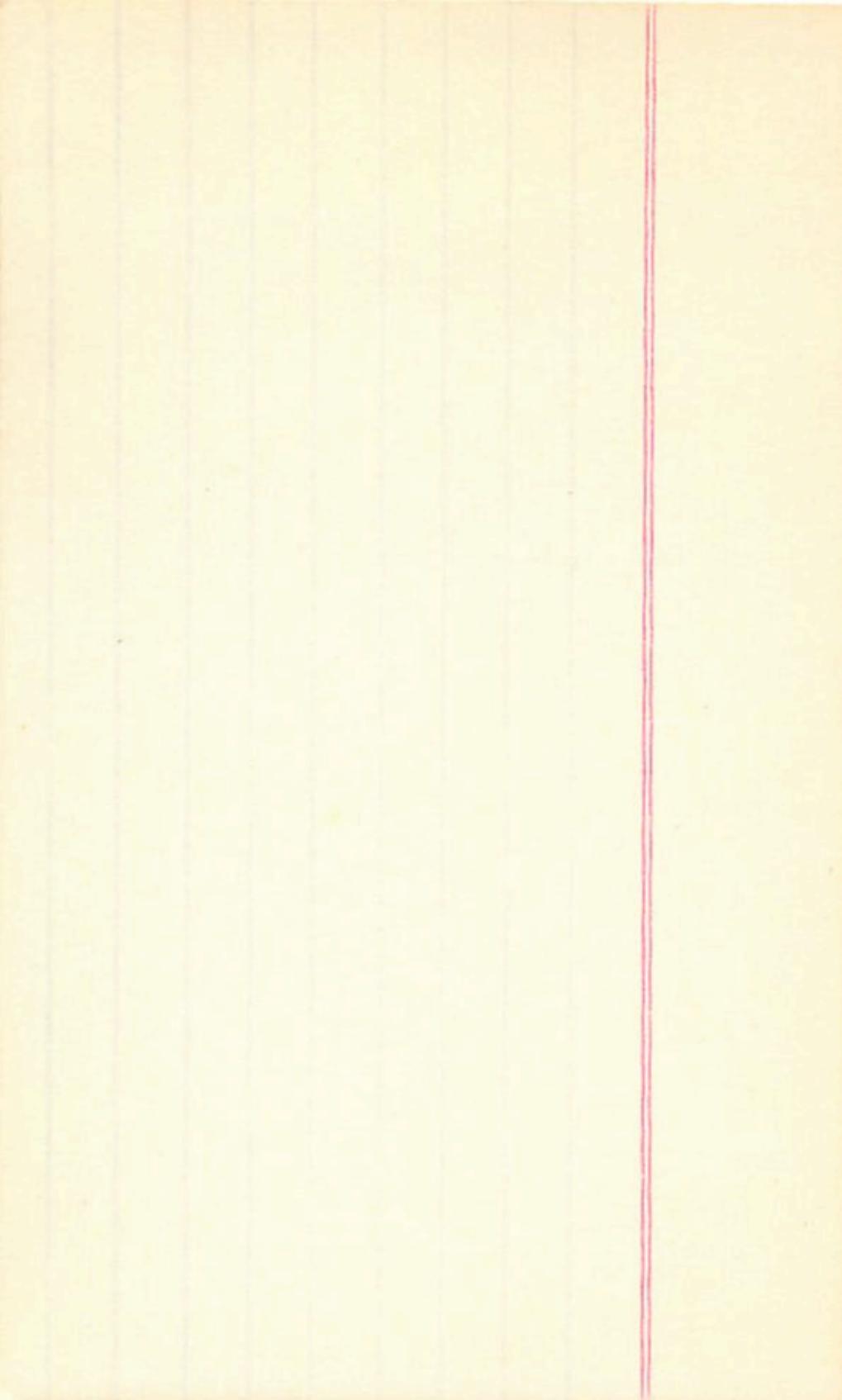
0 31.6 -25 25 11.5

$$\begin{array}{r} 10.58 + 0.58 - 0.01 \quad 0.56 \text{ left} \\ 10.52 + 0.64 - 0.02 \quad 26 \text{ now left} \\ \hline 10.55 + 0.61 - 0.015 \end{array}$$

$$+ 2.5 \quad + 2 \\ 5.65 \quad - 0.33 \\ \hline 5.32 \end{math>$$

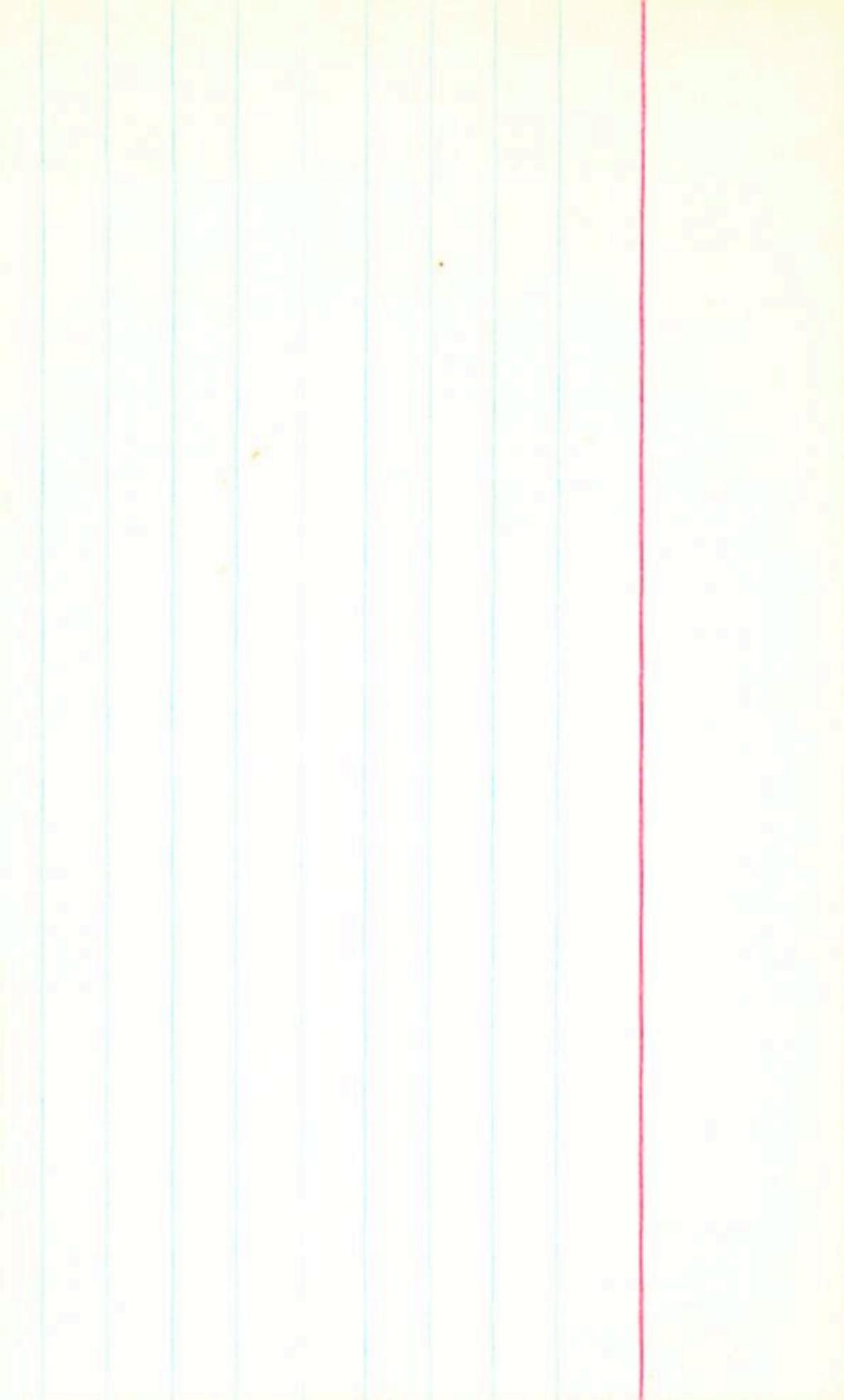
C 700

11000.



46352      00 31 33 → 25      115 054  
75

10.55 + 0.61 = 11.16



1490 +0.67 125

Hu409 0 32.3 -24 22 14.0

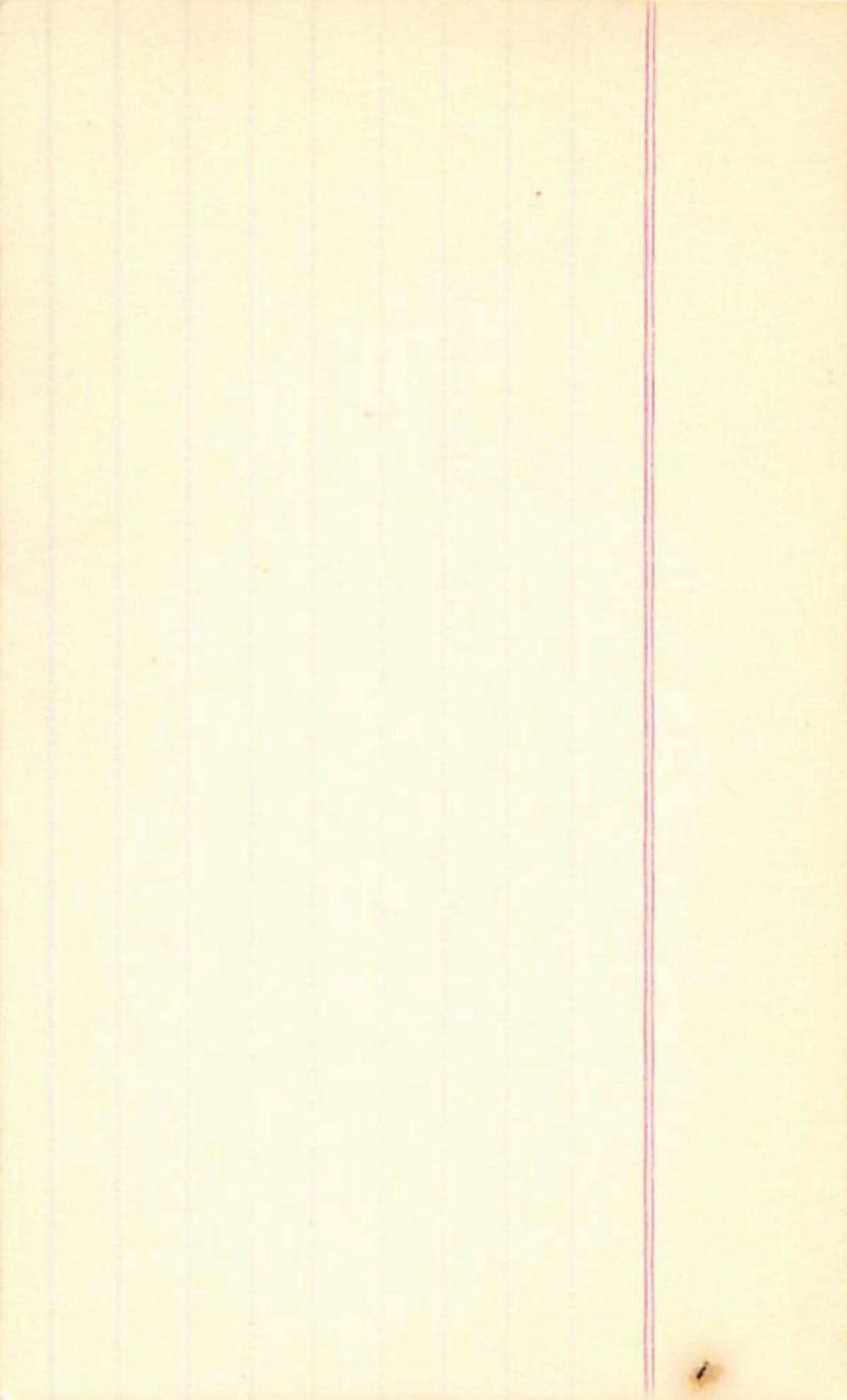
GSDAD

13.65 +0.42 -0.28 26 Oct 67

13.73 +0.38 -0.26  
13.69 +0.40 -0.27

+6 +0.34 -31

120 ✓



46420 ON 32 42 -25 15 13.7

$$\begin{array}{r} 13.45 +0.66 -0.04 \\ \underline{13.45} \quad \underline{+0.67} \quad \underline{+0.16} \\ 13.62 +0.62 -0.04 \\ \hline 13.53 +0.64 -0.04 \end{array}$$

+54 -073 363

